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Heat Transfer Behavior and Physiological Effects of Living Human Skin under Local Radiative Thermal Stimulation

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Abstract

In order to develop a moxibustion treatment device that can heat appropriately by radiation while lowering the risk of burning by the moxa, a local radiative heating device for skin was fabricated and the unsteady response of the skin surface and internal temperature during infrared radiative heating were evaluated based on subjective experiments and numerical analysis. Because it was necessary to perform non-contact temperature measurements of the heated surface to control the heat, methods of evaluating and correcting the impact on measurement precision were studied. The study clarified that as skin was heated, the skin surface temperature rose, and the blood flow speed around the heated part increased. A local thermal sensation corresponded to the increase. Absorption of radiation by skin occurred only near the surface, so it was concluded that a useful way to effectively heat skin, was to set a certain temperature as the upper limit of the surface temperature, and lower the heat when this temperature has been reached, wait for the heat to penetrate more deeply, then restart heating.

Keywords: Radiative heating, Biological heat transfer, Physiological response, Numerical analysis, Subjective experiment.

1. Introduction

Moxibustion treatment, which is an oriental method unlike modern medical treatment, is used as heat treatment to maintain health and to treat diseases [1]. Moxibustion treatment is used to heat acupoints and diseased parts by burning moxa taken from the backs of the leaves of mugwort on the skin to mitigate various symptoms. When skin is thermally stimulated, erythema and localized swelling appear and the skin temperature at the stimulated locations rises [1]. Both the erythema and localized swelling reactions spread widely through bifurcation of axons, so it is said to be a reaction caused by the axon reflex. The axon reflex is expressed even if the medulla of the neurofibroma is severed, so it has been confirmed that it is a reflex that does not pass through the brain, spinal cord or other nerve center. This axon reflex does not occur only on the periphery of the stimulated location; the axon reflex acts at a higher part far from the stimulated part to also be expressed in parts far from the stimulated part. Stimulation of feet or hands occasionally causing the rise of skin temperature on upper and lower limbs is a result of an axon reflex at a higher part far from the stimulated location. Characteristics of moxibustion treatment that can be mentioned are its long history based on practical medical science, the fact that it permits simple treatment without side effects, and its non-invasiveness. But because past moxibustion treatment has been based on facts empirically obtained from subjective statements, there have been almost no cases of the quantitative evaluation of the increase of the temperature of parts heated by moxibustion treatment. It is important to accurately clarify temperature change of heated parts in order to consider the risk of low-temperature burns.

Kimura et al. [2] measured the skin temperature of stimulated parts and skin temperature of the soles of feet by jointly using infrared stimulation and acupuncture stimulation of the interscapulum and pelvic region. The results showed that by also using acupuncture stimulation, the skin temperature of the stimulated part, skin temperature of the soles of the feet, and the deep temperature were each higher than when only infrared stimulation was done. Kimura [3] clarified the fact that the skin sympathetic nerve activity (SSNA) made only a small contribution to change of skin blood flow caused by acupuncture stimulation. Skin sympathetic nerve activity is activity that causes perspiration and encourages a biological reaction in the skin that increases blood flow. Okubo et al. [4] used near-infrared spectroscopy to measure differences in stimulated parts in trapezius muscle during acupuncture stimulation and moxibustion stimulation and the tissue blood volume in the center and outside of the acupoint. The tissue blood volume increased significantly during the period of rest in both the acupuncture stimulation and moxibustion stimulation cases. It showed that the central stimulated part (center of the acupoint) increased significantly more than outside the stimulated part (outside the acupoint). Sato et al. [5] performed a time-series evaluation of blood circulation trends in endocranial blood vessels during indirect moxa treatment of the “gokoku” acupoint (the base part between a thumb and a forefinger on the back side of the hand) by measuring the cerebral blood flow using the Doppler method, discovering that the blood flow increases. Maruyama et al. [6] developed an abdomen heating device that can perform highly precise temperature control, and quantitatively evaluated the heat treatment by performing clinical testing of patients. The

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maximum heating temperature which the patients reported to be comfortable did not appear to be correlated with sex or BMI value, but the older the patient, the higher maximum heating temperature. The internal body temperature distribution during treatment with the abdominal heating control device was calculated by numerical analysis. The results revealed a small increase of the temperature of the internal organs, so it was concluded that the effect of heat treatment was the indirect stimulation of the functions of the internal organs by the action of autonomic nerves. The past research outlined above shows that the greater the quantity of stimulation by heat stimulation, the greater the effectiveness of the treatment. But away from the acupoint, either the stimulation is not very effective or completely ineffective. The change of the blood flow is caused by change of the muscle blood flow during skin stimulation, and it is reported that cerebral blood flows changes during skin stimulation. There is a constant relationship between age and the optimum heating temperature that is considered to be the most comfortable stimulation temperature, and the intervention of an individual thermal sensation is predicted.

This study focused on raises skin temperature by infrared radiation and involved a quantitative evaluation from an engineering perspective including the physiological response done in order to develop an electronic moxibustion device applying thermotherapy. First, using an organism simulation sample, the impact of non-contact method temperature measurement of the surface of the heated part on measurement precision was studied to establish the measurement method. The change over time of the temperature inside the sample was numerically calculated to verify its suitability. Next, using human skin, the non-contact measurement of the surface temperature during radiative heating was quantitatively evaluated. The unsteady response of the skin surface and internal temperature were obtained by a numerical calculation. The physiological response during radiative heating of the skin was also evaluated.

2. Evaluation of Heat Transfer of the Organism Simulation Sample Accompanying Radiative Heating

To develop an electronic moxibustion device, an accurate non-contact method of measuring the surface temperature of a specimen that has been radiatively heated must be established. It is also important to measure the internal temperature of the specimen in order to evaluate effectiveness of indirect moxa treatment and to study safety to prevent burning. This section uses gelatin, which is the organism simulation sample, to analyze factors related to non-contact measurement of the sample surface temperature. And the temperature inside the sample is measured and compared with the numerical simulation to clarify the

characteristics of heat transfer from the surface to the interior of the sample.

2.1 Experimental apparatus and method

Figure 1 shows a schematic diagram of the heating test device. The ceramic heater dimensions are 25[mm] × 25[mm], it is 2mm thick, and it houses an R-typed thermocouple to measure the temperature of the heater. The heater is inserted between two thermocouples with dimensions of 40[mm] × 40[mm] and thickness of 25[mm] (Isowool board, heat resistant temperature of 1,000[°C]) and the surface to be heated is radiated from the heater surface through a hole with section of 22[mm] × 22[mm] formed inside heat-resistant material. Ceramic has low emissivity so it is coated with a heat-resistant black coating. The emissivity of the heater radiative surface is 0.96. On one side of the heat-resistant material, a hole is bored in order to measure the heated surface temperature with an infrared thermometer. Heating is done by electro-conductive heating and radiating the heat from a high-temperature ceramic heater. The temperature of the heater is adjusted to the specified temperature by varying the applied voltage. The temperature of the inside surface of the heat-resistant material is measured using a T-typed thermocouple.

The surface temperature of the heated object was measured using an infrared thermometer (measuring range: 0 to 500[°C], reproducibility: ±0.5[°C]) and a T-typed thermocouple. The radiation temperature sensor was installed at a location where it was directed diagonally toward the heated surface in order to minimize the impact of the high-temperature heater. The measurement area was a range with diameter of about 6mm from around the heated surface. The measurement area of the infrared thermometer could be finely adjusted using an x-axis stage and rotating stage. The heater unit and infrared thermometer were fixed on a single pedestal, and a z-axis stage fixed to this pedestal could integrally adjust the distance from the heated surface. To develop a portable electronic moxibustion device, an infrared thermometer was used to measure the surface temperature.

A heating test was done with gelatin used as the simulation sample. The gelatin concentration was a weight ratio of 1% and it was 20[mm] thick. T-typed thermocouples were installed in the center of the sample at five points in the depth direction. The installation locations were the surface and depths of 2,

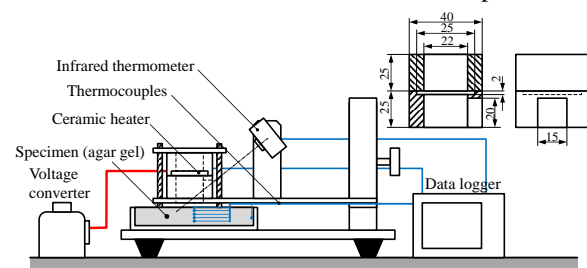


Fig. 1 Schematic of the experimental apparatus (heater unit, temperature measurement device and specimen)

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4, 6, and 8[mm]. The inner wall surface temperature of the container was also measured. The test conditions were heater temperature of 350[°C] and heating time was 20 minutes.

The heater temperature stabilized 10 minutes after the heater was supplied with power. To prevent the sample from being heated during this 10 minute period, a wood panel of thickness 10mm covered with aluminum foil as an insulation material was prepared. After having sandwiched it between a heater unit and samples, the heating of the heater was started. When the heater temperature was achieved to the specified temperature, a shutter was inserted in the lower part of the heater, and a wood panel was removed. The heater unit was brought close to the sample surface, and a shutter was opened afterwards, and the measurement was started.

The output of the infrared thermometer used to measure the surface temperature was also impacted by the energy that the heater and inside wall of the heater reflected from the gelatin. The following is the relational equation for the surface temperature of the sample.

$$\varepsilon_a T_A^4 = \varepsilon'_a T_a^4 + \varepsilon_{heater} (1 - \varepsilon'_a) F_1 T_{heater}^4 + \varepsilon_{wall} (1 - \varepsilon'_a) F_2 T_{wall}^4 \quad (1)$$

Where, ε_a : emissivity set on the infrared thermometer, ε'_a : emissivity of the gelatin, ε_{heat} : emissivity of the heater, ε_{wall} : emissivity of the interior inner wall around the heater, T_A [K]: value measured by the infrared thermometer, T_a [K]: surface temperature of the gelatin, T_{heater} [K]: heater temperature, T_{wal} [K]: inner wall temperature, F_1 : radiation shape factor of heater according to the gelatin, F_2 : radiation shape factor of the inner wall according to the gelatin. For each emissivity, $\varepsilon_a=0.97$ and $\varepsilon_{heater}=\varepsilon_{wall}=0.94$. According to the coefficient of relationship, $F_1=0.164$, if it is assumed that the heated part is enclosed only by the heater and heater inner wall, $F_2=0.836$.

2.2 Numerical analysis

Figure 2 shows the model used for the numerical analysis. The numerical analysis was done assuming that a flat heater with diameter of 20[mm] is installed at a fixed height above the heated surface. Radiation from the heater and its inner wall was presumed to be applied uniformly only to an area with diameter of 20[mm] in front of the heater. It was thought that the heat transport phenomenon is uniform in the circumferential direction around the central axis of the heater, and can be represented axisymmetrically in two dimensions. The temperatures of the heater surface and of the surface of its inner wall were $T_{heater}=350$ [°C] and $T_{wall}=145$ [°C], their emissivity was $\varepsilon_{heater}=0.94$ and it was gray-body radiation. The gelatin was 20mm thick in the depth direction and its interior was uniform. The basic formula used is the following thermal conduction equation. The physiological response such as blood flow and metabolism is not included.

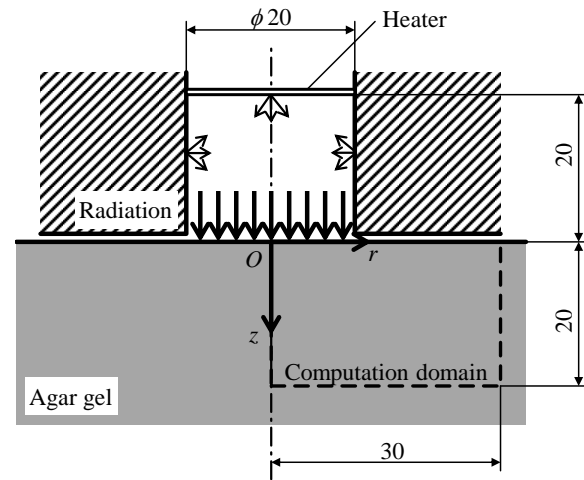


Fig. 2 Numerical analysis model (case of the organism simulation sample)

$$\rho c \frac{\partial T}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left(r k \frac{\partial T}{\partial r} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + q_{rad} \quad (2)$$

Where, ρ [kg/m³]: density of gelatin, c [J/(kgK)]: specific heat of gelatin, T [K]: temperature, t [s]: time, r [m]: distance from the central axis in the radial direction, k [W/mK]: thermal conductivity, z [m]: distance from surface in depth direction. q_{rad} [W/m³] represents the heat generating rate according to radiation absorption, which is found by the following formula.

$$q_{rad} = \sum_i F_i \int_{\lambda_2}^{\lambda_1} \frac{dI_{i\lambda}(z)}{dz} d\lambda = -F \int_{\lambda_2}^{\lambda_1} a_{\lambda} I_{i\lambda}(z) d\lambda \quad (3)$$

Where, F : shape factor of heated surface viewed from heater surface, I_{λ} [W/(m²μm)]: spectral radiation intensity, α_{λ} [1/m]: spectral absorption coefficient, λ [m]: wavelength. The shape factor was set at $F=0.164$ to match test conditions. The spectral absorption coefficient was presumably equal to that of liquid water [7]. The radiation radiated from the heater surface was black-body radiation with temperature T_{heater} , and it conformed to the spectral radiation intensity incident to the sample surface.

The boundary condition on the sample surface was balanced convective heat transfer at the surface and thermal conduction from the surface to the interior of the sample. The air temperature was 18[°C]. It is presumed that radiation from the heater completely penetrates to the interior without being reflected by the surface. In the radial direction of the center axis, it was so-called insulation condition without any temperature gradient. At the bottom edge and circumferential edge in the radial direction of the sample, the temperature was constant. The initial condition was uniform temperature of 18[°C].

As the numerical solution, based on the finite difference method, secondary precision centered differencing was adapted for the diffusion term and the

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full implicit method was adapted to the temporal progress. The difference grid was assumed to be 0.02[mm] from the surface to 0.5[mm], 0.05[mm] to 2[mm], 0.2[mm] to 10[mm] and 0.5[mm] to 20[mm] in the depth direction, and 0.2[mm] at equal intervals in the radial direction. The total number of grids in the depth direction was 112. The time interval was assumed to be 0.001s. The gelatin density ρ , specific heat c , and thermal conductivity k were 1.00×10^3 [kg/m³], 4.15×10^3 [kJ/kg], and 0.607 [W/mK] respectively [8].

2.3 Results and discussion

Figure 3 shows the measurement results. The gelatin surface was heated, raising its temperature to 35[°C]. The measurement values obtained by the infrared thermometer were nearly 15[°C] higher than those obtained by the thermocouples. When the surface temperature was obtained by Eq. (1) assuming the emissivity of the gelatin was $\epsilon'_a=0.97$, it differed from the value measured by the thermocouples by about 3[°C]. Figure 4 shows the results in the case

where the gelatin's emissivity ϵ'_a is varied. This shows that if it is assumed that $\epsilon'_a = 0.965$, it conforms to the values measured by the thermocouples. Figure 5 compares the measurement results and calculation results. The thermal conductivity of the surface impacts the results of the calculation of the surface temperature, so the heat transfer coefficient was decided so that the change over time of both surface temperatures conformed most closely. The thermal conductivity that was decided is 26.2[W/(m²K)]. This revealed that numerical calculation can generally reproduce change over time of the surface temperature. Figure 6 shows a comparison of measurement results with calculated results for change over time of the temperature distribution inside the gelatin layer. It shows that the two temperature distributions roughly conform. It is suggested that the difference depends on the uncertainty of thermophysical properties of the sample such as specific heat. It also reveals that change over time of the temperature inside the layer is large near the surface, but below a constant depth, almost no change of the temperature can be seen.

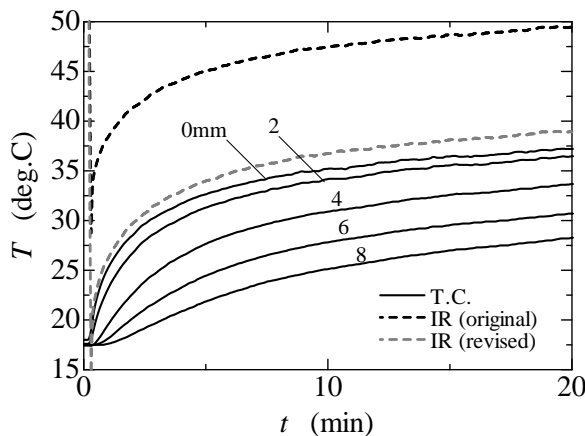


Fig. 3 Results of measurements of change over time of the surface and interior temperature of the organism simulation sample (gelatin) (comparison of surface temperature measured by the thermocouples and infrared thermometer)

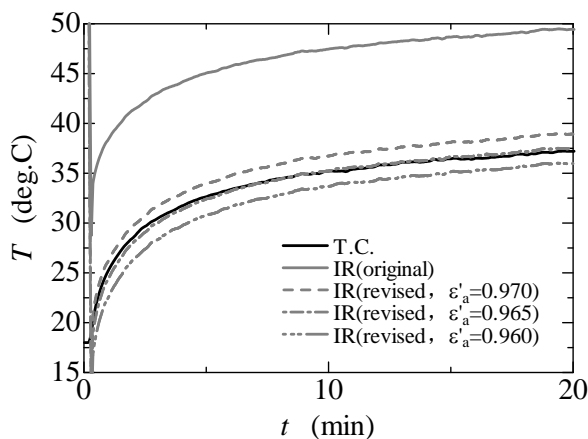


Fig. 4 Impact of emissivity of the organism simulation sample (gelatin) on skin temperature obtained from values measured by the infrared thermometer

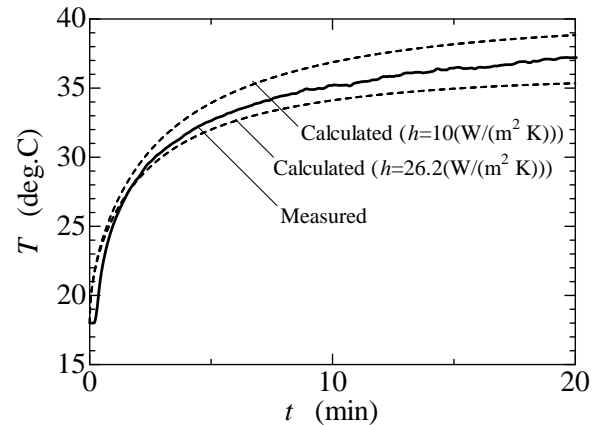


Fig. 5 Comparison of measurement results and calculation results of change over time of surface temperature of the organism simulation sample (gelatin)

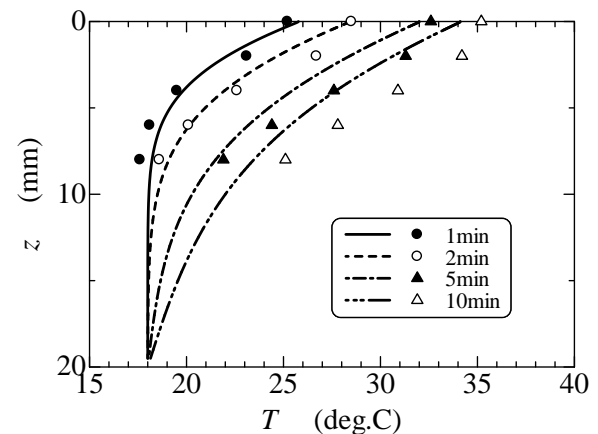


Fig. 6 Comparison of measurement results and calculation results of change over time of temperature distribution in the organism simulation sample (gelatin)

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3. Evaluating the Surface Temperature Measurements and Physiological Response of Human Skin Accompanying Radiative Heating

This section evaluates the increase of skin temperature and physiological response when human skin was radiatively heated based on testing using human subjects and on numerical calculations.

3.1 Experimental method

The heating test device is the same as that shown in Fig.1. To confirm the method of obtaining the skin temperature based on the infrared thermometer, a test heating of the subject's palm was done at heater temperature of 350[°C]. The skin temperature was obtained according to the output from the infrared thermometer in the same way as explained in the previous chapter. Figure 7 shows the test results. The skin temperature was raised to almost 48[°C] by the heating. The skin temperature obtained by the infrared thermometer was found to conform almost perfectly to the skin temperature measured by the thermocouples.

Heating was done until the subject felt heat pain in order to stimulate the nervous system in the skin to simulate actual moxibustion treatment. Therefore, heating started then ended when the subject felt heat pain. The decision to end heating was, therefore, made when the subject reported feeling heat pain. As testing time, the subject was observed in resting state for 5 minutes, then heating was started. And assuming the heating time and observation time was 10 minutes, the

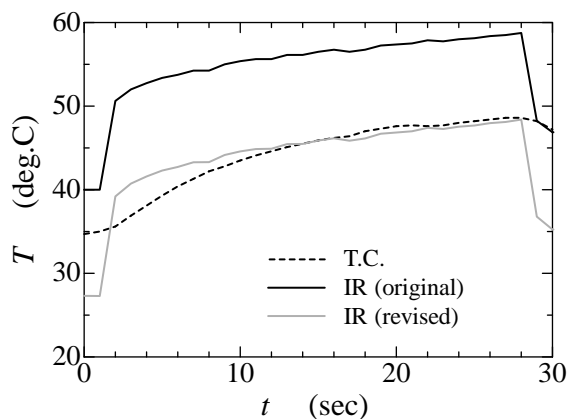


Fig. 7 Comparison of change over time of human skin surface temperature measured by thermocouples and by the infrared thermometer

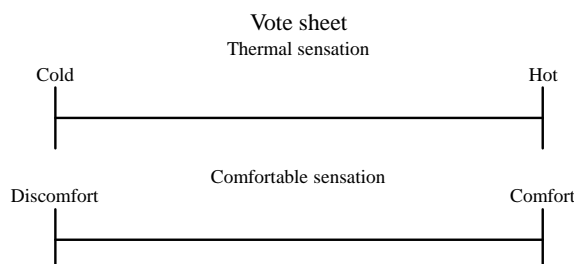


Fig. 8 Local thermal sensation and comfort report table

total test time was 15 minutes. Four subjects were tested, with each tested three times to evaluate individual differences in the thermal response and physiological response of their skin. All the subjects were healthy men in twenties and were medium flesh and height. The heater temperature was 350[°C]. The center of the trapezius muscle on the shoulder was heated. The items measured were the skin temperature of the heated part, blood flow speed around the heated part, average skin temperature (forehead, brachium, back of hand, abdomen, thigh, lower leg, top of the feet), deep temperature, heart rate, local thermal sensation, comfort, air temperature, and relative humidity. The measuring instruments used were an infrared thermometer, a rheometer, a thermistor skin thermometer, an ear thermometer, a heart rate monitor, and subjective reports (local thermal sensation, comfort), a thermometer and a hygrometer. The measurements were made at intervals of 0.5 seconds, and subjective reports given at intervals of 5 minutes. The average skin temperature was obtained by Hardy-Dubois' 7-point method [9]. A subjective report table is shown in Fig. 8. The subjects were asked to record thermal sensation and comfort state at the reporting time on the lines in the lined part of the report table, then based on ASHRAE's thermal sensation indices[10], the thermal sensation was converted to -3(cold) to +3 (hot) and comfort was converted to -2 (uncomfortable) to +2 (comfortable).

3.2 Numerical analysis

It is important to predict the temperature distribution on and under the skin surface in order to lower the risk of burning on the skin surface, and it is necessary in order to perform heat control to transfer heat into the skin. The heat transfer behavior to and inside the skin surface were analyzed by numerical analysis and the results were compared with the experimental results.

Figure 9 shows the analysis model. The calculation area is a rectangular area from the skin surface to 5[mm] deep in the muscle layer in the depth direction and 30[mm] from the center axis in the radial direction. The heater is handled in the same way as it was during numerical analysis using gelatin. The temperature and emissivity of the surfaces of the heater and its inner wall were $T_{heater} = 350[°C]$, $\epsilon_{heater}=0.94[-]$, $T_{wall}=145[°C]$, and $\epsilon_{wall}=0.94[-]$ respectively. The radiation from the surfaces of the heater and its inner wall was gray-body. The phenomenon assumed to be reproduced axisymmetrically in two dimensions. The following biological heat transfer formula of Pennes [11] is applied as the basic equation.

$$\rho c \frac{\partial T}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left(rk \frac{\partial T}{\partial r} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \rho_b c_b \omega_b (T_a - T) + q_{met} + q_{rad} \quad (4)$$

Where, ρ [kg/m³] and ρ_b [kg/m³] are the density of the skin and blood, c [J/(kgK)] and c_b [J/(kgK)] are the

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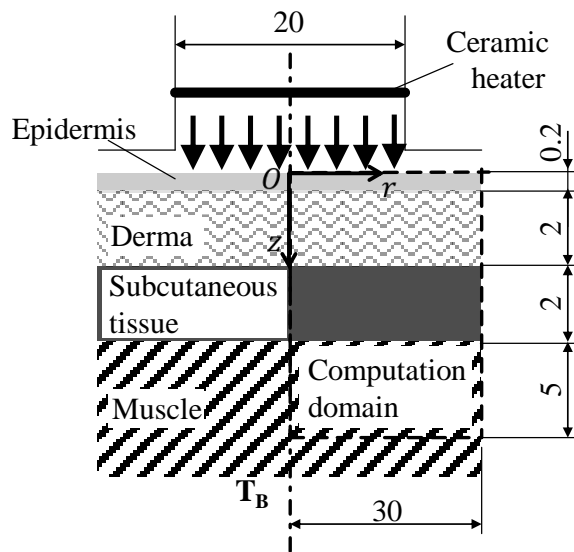


Fig. 9 Numerical simulation model (case of human skin)

specific heat of the skin and blood, T [K] is the skin temperature, k [W/mK] is the thermal conductivity of the skin, T_a [K] is the arterial temperature, ω_b [$\text{m}^3/(\text{s}\cdot\text{m}^3)$] is the blood perfusion rate, and q_{met} [W/m³] is the metabolism. The radiation absorption of the skin is assumed to be based on liquid water. The heat generating rate q_{rad} [W/m³] of radiative absorption can be obtained by Eq. (3). As the structure of the skin in the depth direction, four layers, epidermis, derma, subcutaneous tissue, and muscle, were considered shown in Fig.9. The thicknesses of the epidermis, derma, and subcutaneous tissue layers were assumed to be 0.2mm, 2mm, and 2mm respectively. Thermophysical properties and quantities of state of skin are shown in Table 1 [11,12]. It is assumed that the biological materials constituting each layer are isotropic, and for tissue other than epidermis and for tissue under the derma, metabolism and blood perfusion respectively were considered. It was assumed that metabolism q_{met} is identical in all layers at 4,200[W/m³], and that physical properties and blood perfusion rate were not temperature dependent.

The boundary condition on the surface is balanced convective heat transfer at the surface and thermal conduction to the interior. Deep boundary condition was the deep temperature T_B [K] given as a constant value. T_B is obtained by the following equation.

$$T_B = T_a + \frac{q_{\text{met}}}{\rho_b c_b \omega_b} \quad (5)$$

The arterial temperature T_a was 38[°C]. If the air temperature is considered to be 25[°C], the initial values of the skin surface and deep temperature before heating are 36.2[°C] and 38.2[°C] respectively. Initial conditions are steady state before heating and one-dimensional temperature distribution in the depth direction. The boundary on the outside in the radial

Table 1 Thermophysical properties and blood perfusion rate of each layer of skin [11,12]

	Heat conductivity (W/(m·K))	Specific heat J/(kg·K)	Density (kg/m ³)	Blood perfusion rate (m ³ /(s·m ³))
Epidermis	0.45	3300	1200	0.0
Dermis	0.45	3300	1200	1.3×10^{-3}
Adipose tissue	0.27	3100	950	5.0×10^{-4}
Muscle	0.50	3465	1050	9.0×10^{-4}
Blood	0.51	3720	1060	---

direction is fixed to its temperature distribution. The temporal interval Δt was set as 0.0001[s], the spatial interval Δz was 0.02[mm] for the epidermis and derma, 0.1[mm] for subcutaneous tissue, and 1mm for muscle.

3.3 Results and discussion

Figure 10 shows change over time of skin temperature and blood flow speed obtained by the second test on subject C. The blood flow speed was measured at the skin surface by a Doppler rheometer. The defined blood flow rate or the blood perfusion rate used in the numerical simulation cannot be measured. Figure 11 shows the correlation of heating time with skin temperature increase, and Fig. 12 shows the correlation of heating time with blood flow speed increase for three tests of all four subjects. The skin temperature increase and blood flow speed increase values represent maximum increase values after heating. These appearance times were the heating end time for the skin temperature and approximately one minute later of the heating end for the blood flow speed. Figure 10 shows that the skin temperature and blood flow speed both increased at the same time as heating. The heating time in this case is 30 seconds, and after heating was stopped, the skin temperature fell rapidly, but the rise of blood flow speed continued, showing that it takes much longer than the heating time for the blood flow speed to return to its state before heating. Figure 11 shows that the average skin temperature increase of subject A is slightly higher than that of other subjects. The thermal ache of subject A was assumed to be higher. Therefore heating time of subject A was longer than other subjects. The rise rate

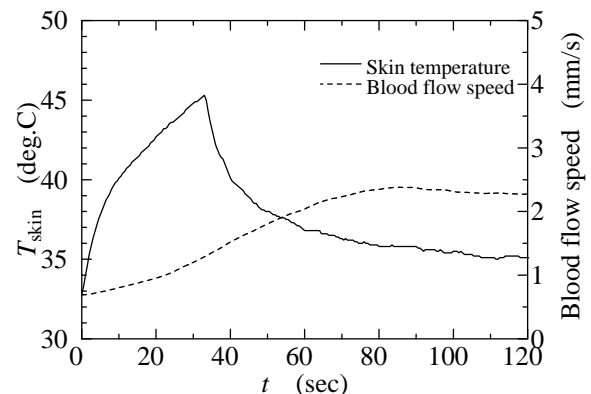


Fig. 10 Change over time of skin temperature and blood flow speed

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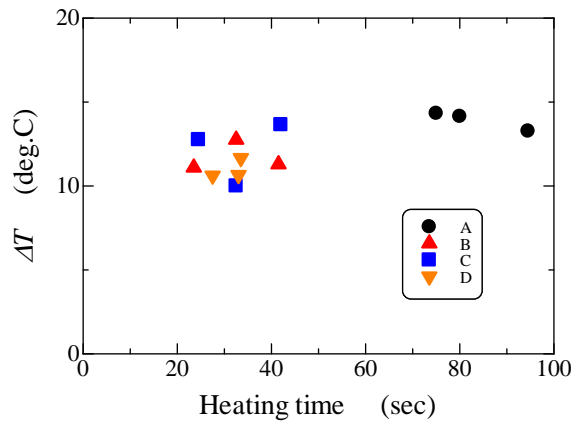


Fig. 11 Correlation of heating time with skin temperature increase

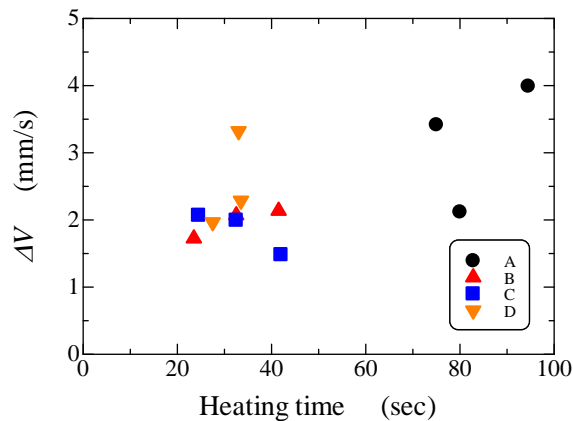


Fig. 12 Correlation of heating time with blood flow speed increase

in skin temperature of prolonged time was not so large. Figure 12 shows that if the heating time is long, the blood flow speed around the heated part increases greatly. It can be concluded that the blood flow speed is increased by the heat stimulation on the skin reaching the nerve system. And erythema that is often seen during real acupuncture and moxibustion treatment was actually seen during the test. And no significant differences between the average skin temperature and deep temperature were observed. Figures 13 and 14 show change over time of local thermal sensation and comfort respectively. The data of one subject whom the local thermal sensation fell down after heating were removed. These values signify a difference from the state before heating. They show that after heating starts, subjects feel heat and their comfort increases. These changes of state are seen to continue for some time even after heating is stopped.

Figure 15 compares measurement and calculation results. It shows that calculated skin temperature is higher than measured skin temperature. So the specific heat and density of the epidermis and derma used for the calculation were varied. As a result of this operation, the calculated results confirmed to the

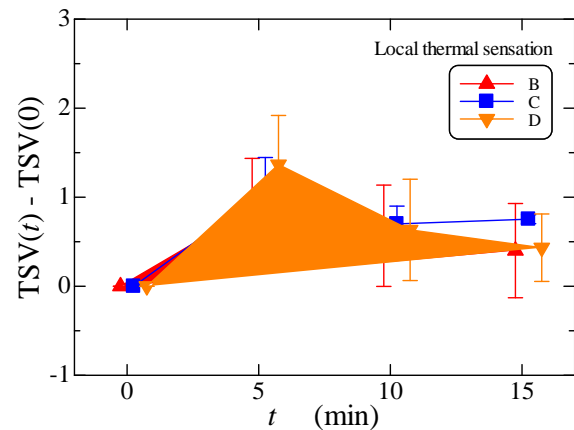


Fig. 13 Change over time of local thermal sensation

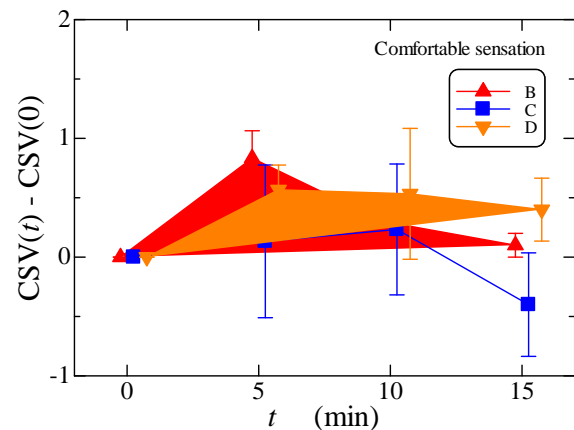


Fig. 14 Change over time of comfort

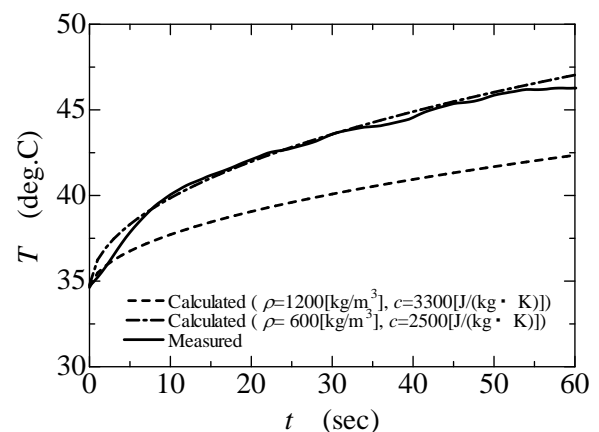


Fig. 15 Comparison of measurement results and calculation results of change over time of surface temperature of human skin

measured results. It can be concluded that accurate thermophysical properties of skin are very important. However, it is difficult to measure the thermophysical properties of each skin layer in vivo. These values are influenced by individual difference and physical condition. Figure 16 shows a vertical distribution of heat generating rate by radiation absorption. It shows

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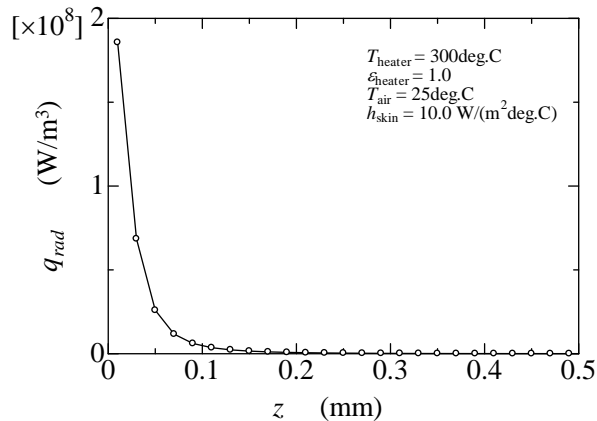


Fig. 16 Vertical distribution of heat generating rate by radiation absorption

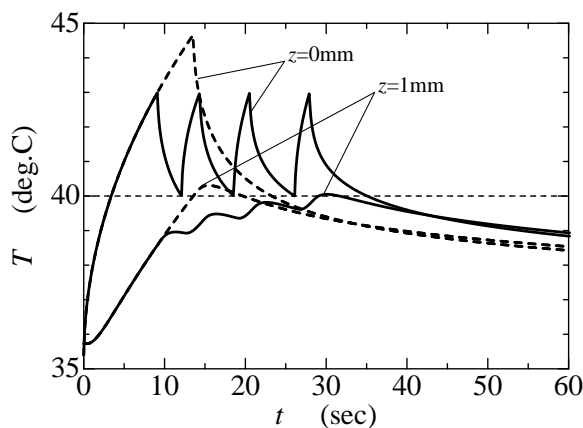


Fig. 17 Change over time of temperature distribution of skin layer under repetitive heating

that the heat generating rate near the surface is high, and the heat generating rate inside the skin tends to decline abruptly. Figure 17 shows change over time of temperature distribution of skin layers when repetitive heating was done. The heater and wall temperatures were assumed to be 450 and 188[°C], respectively. The thermal ache was assumed to occur at 40[°C]. When the inner temperature at 1mm in depth reached 40[°C], heating was finished. In the case of repetitive heating, when the skin temperature became 43[°C], heating was stopped, and heating was reopened when it returned to 40[°C]. Heating was performed repeatedly until the inner skin temperature at 1mm in depth reached 40 [°C]. The inner skin temperature raises while avoiding overheat at the skin temperature by heating repeatedly. The inner temperature drop is relaxed after heating, too. To the deeper position, it is thought that heat is conveyed. Judging from observations of thermotherapy, the rise of the skin temperature at a constant depth is important. It clarified that to avoid burning, it is necessary to hold down the increase of the skin temperature, and to realize temperature increase inside the skin, it is necessary to perform repetitive heating.

4. Conclusions

Heating tests of organism simulation samples and human skin using infrared radiation were done accompanied by numerical calculations. Their impact on measurement precision of non-contact type temperature measurements of heated skin was studied. Numerical calculations of change over time of temperature of the surface and interior were done, verifying their suitability. And the physiological response to skin radiation heating was evaluated. The results obtained are summarized below.

- (1) The non-contact measurements of surface temperature using an infrared thermometer obtained results identical to contact measurements by considering the radiation transfer from the surroundings and radiation properties of the specimen.
- (2) It showed clearly that in the case where a numerical calculation of radiative heating of skin was performed, the thermophysical properties of each tissue of the skin had a great impact on the calculation results. Radiation absorption of skin was limited to near the surface, and heat transfer by thermal conduction to the inside of the skin was predicted.
- (3) Blood flow speed increased along with skin heating. This was a result of axon reflex acting under heat stimulation to the nervous system of the skin, causing erythema. And this impact continued for a fixed period even after heating was stopped. The results of subjective reports of local thermal sensation and comfort also conform to this.
- (4) Repetitive heating is an effective way to mitigate the possibility of burning caused by the increase of skin temperature and to increase the temperature of affected part inside the skin as thermotherapy.

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